

## V Closure Models, an Overview

Last lecture we saw that in attempting to "solve" turbulence we uncovered a closure problem whereon  $\partial_t \langle u_i u_j \rangle \sim \nabla \cdot \langle u_i u_j u_k \rangle$ . This time we will examine the problem in more detail and various closure models that have been developed. All of these models are ad hoc and should be taken with a (large) grain of salt. They are all wrong, but given enough adjustable parameters, they can be made to work well.

As usual, let's start with the NS eqn

$$\frac{\partial \vec{U}}{\partial t} + \vec{U} \cdot \nabla \vec{U} = -\nabla P + \nu \nabla^2 \vec{U} \quad \textcircled{1}, \text{ where } \vec{U} = \underbrace{\vec{U}_0}_{\text{mean}} + \underbrace{\vec{u}}_{\text{fluctuating}}$$

$$P = p_0 + p, \quad \nu \nabla^2 \vec{U} = \nabla \cdot (2\nu \underline{\underline{S}}), \quad \underline{\underline{S}} = \frac{1}{2} [(\nabla \vec{U}) + (\nabla \vec{U})^T],$$

$\underline{\underline{S}}$  is the rate of strain tensor, and  $\underline{\underline{S}} = \underline{\underline{S}}_0 + \underline{\underline{s}}$ .

$$\text{Averaging } \textcircled{1} \quad \frac{\partial \vec{U}_0}{\partial t} + \vec{U}_0 \cdot \nabla \vec{U}_0 = -\vec{\nabla} p_0 + \nabla \cdot (2\nu \underline{\underline{S}}_0 + \langle \vec{u} \vec{u} \rangle)$$

$\langle \vec{u} \vec{u} \rangle$  is the 2<sup>nd</sup> order 1 point correlation function from the last lecture,  $C_{ij}(0)$ . This term,  $\langle u_i(\vec{x}) u_j(\vec{x}) \rangle$  is often called the Reynolds stress,  $R_{ij}$ .

$$\text{So, we have } \frac{\partial \vec{U}_0}{\partial t} + \vec{U}_0 \cdot \nabla \vec{U}_0 = -\vec{\nabla} p_0 + \nabla \cdot (2\nu \underline{\underline{S}}_0 + \underline{\underline{R}}). \quad \textcircled{2}$$

the mean flow depends on the turbulence through a second order moment. So, we need an equation for  $\underline{\underline{R}}$

Subtracting ①-② yields

$$\frac{\partial \bar{\mathbf{u}}}{\partial t} + \bar{\mathbf{u}}_0 \cdot \nabla \bar{\mathbf{u}} + \bar{\mathbf{u}} \cdot \nabla \bar{\mathbf{u}}_0 + \nabla \cdot (\bar{\mathbf{u}} \bar{\mathbf{u}} - \underline{\underline{\mathbf{R}}}) = -\nabla p + \nu \nabla^2 \bar{\mathbf{u}}$$

$$\text{So, } \partial_t (u_i u_j) = u_j \partial_t u_i + u_i \partial_t u_j = -u_j u_{0k} \partial_k u_i - u_i u_{0k} \partial_k u_j$$

$$-u_j u_k \partial_k u_{0i} - u_i u_k \partial_k u_{0j} - u_j \partial_k (u_k u_i) - u_i \partial_k (u_k u_j) + u_j \partial_k R_{ik} + u_i \partial_k R_{jk} - u_j \partial_i p - u_i \partial_j p + \nu (u_i \nabla^2 u_j + u_j \nabla^2 u_i)$$

Averaging this and simplifying leads to

$$\partial_t \underline{\underline{\mathbf{R}}} + \bar{\mathbf{u}}_0 \cdot \nabla \underline{\underline{\mathbf{R}}} + \underline{\underline{\mathbf{R}}} \cdot \nabla \bar{\mathbf{u}}_0 + (\underline{\underline{\mathbf{R}}} \cdot \nabla \bar{\mathbf{u}}_0)^T + \nabla \cdot (\bar{\mathbf{u}} \bar{\mathbf{u}} \bar{\mathbf{u}}) = 2 \langle p \underline{\underline{\mathbf{S}}} \rangle + \nabla \langle p \mathbf{u} \rangle + (\nabla \langle p \mathbf{u} \rangle)^T + \nu \nabla^2 \underline{\underline{\mathbf{R}}} + 2\nu \langle (\partial_k \bar{\mathbf{u}}) (\partial_k \bar{\mathbf{u}}) \rangle \quad \textcircled{3}$$

and we see that the equation for  $\underline{\underline{\mathbf{R}}}$  depends on third order moments,  $\nabla \cdot (\bar{\mathbf{u}} \bar{\mathbf{u}} \bar{\mathbf{u}})$ . Note that equation ①-③ display the closure problem using 1 pt statistics. Last lecture we developed the equations for 2 pt statistics, which we will revisit shortly.

Let us now explore a simple 1 pt closure. Note that 1 pt closures are sometimes referred to as "engineering" closures since they typically prescribe a model for  $\underline{\underline{\mathbf{R}}}$  and thus only provide information about the mean flow, which is often sufficient for engineering purposes.

The basis for most of these closures was introduced by Boussinesq in 1887

$$-\underline{\underline{\mathbf{R}}} = 2\nu_T \underline{\underline{\mathbf{S}}}_0 - \frac{2}{3} \rho \underline{\underline{\mathbf{I}}} E, \text{ where } E = \frac{1}{2} \langle \mathbf{u}^2 \rangle \text{ is the familiar kinetic energy, } \underline{\underline{\mathbf{S}}}_0 \text{ is the mean rate of strain tensor and } \nu_T \text{ is a prescribed coefficient. } \nu_T \text{ is typically interpreted}$$

as an eddy viscosity because inserting this closure

$$\frac{\partial \vec{u}_0}{\partial t} + \vec{u}_0 \cdot \nabla \vec{u}_0 = -\nabla (p_0 + \frac{2}{3} E) + \nabla \cdot [2(\nu + \nu_T) \underline{\underline{S}}_0]$$

A simple estimate for  $\nu_T = \langle u^2 \rangle^{1/2} L_m$ , where  $L_m$  is the mixing length, which can be experimentally determined.  $L_m$  is analogous to the mean free path but for a fluid parcel. This simple estimate works passably well sometimes, but obviously fails if for instance the turbulence is anisotropic. More advanced models such as Spalart-Allmaras, k- $\epsilon$ , and k- $\omega$  models employ different and more complex estimates for  $\nu_T$ , but they all only work well for specific cases, and none of these actually solve for turbulent quantities.

So, let's now move on to the two point version of (3), which we derived last time (dropping the divergence term)

$$\frac{1}{2} \partial_t C_{ii} = \frac{\partial}{\partial r_k} C_{ik,i} + \nu \nabla^2 C_{ii} \quad (4)$$

Schematically, this is simply

$$\partial_t \langle uu \rangle = \langle uuu \rangle + \nu \langle uu \rangle \quad (5)$$

The third order equation is

$$\partial_t \langle uuu \rangle = \langle uuuu \rangle + \langle uup \rangle + \nu \langle uuu \rangle, \text{ but}$$

$p$  can be computed by taking the divergence of the NS eqn,  $p(\vec{x}') = \frac{1}{4\pi} \int \frac{1}{|\vec{x} - \vec{x}'|} \frac{\partial^2 u_m u_n}{\partial x_m \partial x_n} d\vec{x} \Rightarrow$

$$\partial_t \langle uuu \rangle = \langle uuuu \rangle + \int \langle uuuu \rangle + \nu \langle uuu \rangle \quad (6)$$

The first 2pt closure we'll explore (and revisit later)

page 4 closure assumes that the 2pt joint PDF of  $u$  is Gaussian  $\rightarrow$

Gaussian PDFs of  $u \Rightarrow$  that  $u_i(\vec{x})$  and  $u_j(\vec{x}')$  are statistically independent.

This is approximately true for well separated ( $r \gg L$ ) points but, usually,  $\textcircled{4}$

not true at smaller scales. Nonetheless, Millionshtchikov proposed

such a closure in 1941, where  $\textcircled{5}$  and  $\textcircled{6}$  are kept in

their exact form and  $\langle u_i u_j u_k u_l \rangle$  is approximated as

$$\langle u_i u_j \rangle \langle u_k u_l \rangle + \langle u_i u_k \rangle \langle u_j u_l \rangle + \langle u_i u_l \rangle \langle u_j u_k \rangle$$

due to the QN assumption. A different way to state this is that the 4<sup>th</sup>

order cumulants are zero. This approach closes the system, but

it has some serious deficiencies. First, the system is

time reversible, which is inconsistent with turbulence. Second,

as the system evolves, the energy spectrum develops large,

negative portions, which is unphysical. Refinements to QN

can be incorporated, and we will discuss them shortly.

To do so, we need to move over to Fourier space.

Recall that  $C_{ij}(r)$  and  $C_{ik,j}$  are each

functions of single scalar functions, e.g.,

$$\frac{1}{2} C_{ii}(r) = C(r) \quad \text{and} \quad C_{ik,i} = D(r) \hat{r}_k$$

$\therefore \textcircled{4}$  can be rewritten as simply

$$\partial_t C(r) = \frac{1}{r^2} \frac{\partial}{\partial r} [r^2 D(r)] + 2\nu \nabla^2 C(r) \quad \textcircled{7}$$

This is one way to write the von Karman-Howarth

equation mentioned but not written last time.

Before going further with the closure discussion, we

need to convert  $\textcircled{7}$  to Fourier space.

page  $\textcircled{8}$  Wind tunnel experiments do have quasi-Gaussian PDFs

$$u_i(\vec{k}) = \int d\vec{x} e^{-i\vec{k}\cdot\vec{x}} u_i(\vec{x})$$

$$u_i(\vec{x}) = \int \frac{d\vec{k}}{(2\pi)^3} e^{i\vec{k}\cdot\vec{x}} u_i(\vec{k})$$

$$\Rightarrow \langle u_i(\vec{k}) u_j(\vec{k}') \rangle = \int d\vec{x} \int d\vec{x}' e^{-i\vec{k}\cdot\vec{x} - i\vec{k}'\cdot\vec{x}'} \underbrace{\langle u_i(\vec{x}) u_j(\vec{x}') \rangle}_{C_{ij}(\vec{r})}$$

$$= \underbrace{\int d\vec{r} e^{-i\vec{k}\cdot\vec{r}} C_{ij}(\vec{r})}_{C_{ij}(\vec{k})} \underbrace{\int d\vec{x}' e^{-i\vec{x}'\cdot(\vec{k}+\vec{k}')} (2\pi)^3 \delta(\vec{k}+\vec{k}')}_{(2\pi)^3 \delta(\vec{k}+\vec{k}')}$$

$$\therefore \langle u_i(\vec{k}) u_j(\vec{k}') \rangle = C_{ij}(\vec{k}) (2\pi)^3 \delta(\vec{k}+\vec{k}')$$

Isotropy & parity  $\Rightarrow$  because of homogeneity

$$C_{ij}(\vec{k}) = A(k) \hat{k}_i \hat{k}_j + B(k) \delta_{ij}, \quad \hat{k}_i = \frac{k_i}{k}$$

Incompressibility  $\Rightarrow k_i C_{ij} = 0 \Rightarrow B = -A$

$$\text{or } C_{ij}(\vec{k}) = B(k) (\delta_{ij} - \hat{k}_i \hat{k}_j)$$

Note that  $\frac{1}{2} C_{ii} \leq B(k)$  and

$$E = \frac{1}{2} \langle u^2 \rangle = \frac{1}{2} \int C_{ii}(\vec{k}) e^{i\vec{k}\cdot\vec{0}} d\vec{k} = \int B(k) d\vec{k} = \int_0^\infty 4\pi k^2 B(k) dk$$

but this means that  $B(k) = E^{(3)}(k)$ , the 3D energy spectrum or that  $4\pi k^2 B(k) = E(k)$ , the 1D energy spectrum.

$$\therefore C_{ij}(\vec{k}) = \frac{E(k)}{4\pi k^2} (\delta_{ij} - \hat{k}_i \hat{k}_j)$$

Now, Fourier transforming (7) with the above derivation and some algebra the spectral version of the von Karman-Howarth equation emerges

$$\partial_t E(k) = T(k) - 2\nu k^2 E(k),$$

where  $T$  is basically the Fourier transform of

$$\frac{1}{r^2} \frac{\partial}{\partial r} [r^2 D(r)] \text{ and is called the spectral$$

kinetic energy transfer function. Alternatively, we

$$\text{could write } \partial_t E = - \frac{\partial \Pi}{\partial k} - 2\nu k^2 E, \text{ where}$$

$\bar{\pi} = - \int_0^k T(k) dk = \int_k^\infty T(k) dk$  is the spectral kinetic energy flux and represents the net transfer of energy from all eddies with  $k' < k$  to wavenumbers  $k'' > k$  —  $\bar{\pi} = \epsilon$  in the inertial range. So, now that we are in Fourier space, rather than looking for a closure that relates  $\langle u u u \rangle$  to  $\langle u u \rangle$ , we want a relationship between  $T(k)$  and  $E(k)$  or a dynamical equation of the form  $\partial_t T(k) = \dots$ . The former are called algebraic closures and the QN closure is an example of the latter. Let's first look at some algebraic closures.

Algebraic closures are constructed to guarantee that the correct inertial range spectrum is recovered. So, in that sense, they all work well, but all of the early closures, e.g., Obukhov (1941), Ellison (1961), and Heisenberg (1948), all suffered from the obvious deficiency that  $\pi$  depended on a large range of  $k$ . For instance, Heisenberg (1948) proposed

$$\pi = \alpha \left( \int_k^\infty k^{-3/2} E^{1/2} dk \right) \left( \int_0^k k^2 E dk \right)$$

This obviously violates locality in wavenumber. The most successful of these closures is due to Pao (1965)

$$\pi = \alpha e^{1/3} k^{5/3} E$$

This closure actually works quite well. It is local and produces an energy spectrum

$$E = \alpha e^{2/3} k^{-5/3} \exp \left[ -\frac{3\alpha}{2} \left( k/k_d \right)^{4/3} \right], \text{ which works}$$

in both the inertial range and dissipation range.

the Pao model even works relatively well at predicting the spectrum for scales  $k \leq 1/h$ . But, the Pao model fails to accurately predict things like the skewness and flatness of the velocity PDFs. So, let's now revisit and improve on the QN closure introduced earlier. As before, we'll retain the exact 2<sup>nd</sup> order equation

$$\frac{\partial E}{\partial t} = T - 2\nu k^2 E \quad \text{and the 3<sup>rd</sup> order eqn}$$

which is of the form  $\frac{\partial T}{\partial t} = NL$  terms + viscous terms

So, let's now derive the 3<sup>rd</sup> order eqn, but first we need some notation.

the 3<sup>rd</sup> order, 3 point velocity correlation tensor

$$C_{i,j,k}(\vec{r}, \vec{r}') = \langle u_i(\vec{x}) u_j(\vec{x}') u_k(\vec{x}'') \rangle = \langle u_i u_j' u_k'' \rangle$$

$\vec{r} = \vec{x}' - \vec{x}$  and  $\vec{r}' = \vec{x}'' - \vec{x}$ . The Fourier x form

of  $C_{i,j,k}(\vec{r}, \vec{r}')$  is

$$\Phi_{i,j,k}(\vec{k}, \vec{k}') = \frac{1}{(2\pi)^6} \iint C_{i,j,k} e^{-j(\vec{k} \cdot \vec{r} + \vec{k}' \cdot \vec{r}')} d\vec{r} d\vec{r}'$$

and we can write  $T$  in terms of  $\Phi_{i,j,k}$  as

$$T = 4\pi k^2 k_j \int \Phi_{i,j,k}(\vec{k}, \vec{k}') d\vec{k}'. \quad \text{the NS eqn } \Rightarrow$$

$$[\partial_t + \nu(k^2 + k'^2 + k''^2)] \Phi_{i,j,k} = \text{Transform}[\langle u u u u \rangle], \quad \text{where}$$

$\vec{k} + \vec{k}' + \vec{k}'' = 0$ . Using the QN hypothesis (and a lot of

algebra) one finds

$$[\partial_t + \nu(k^2 + k'^2 + k''^2)] \Phi_{i,j,k} = P_{ikl}(\vec{k}'') \Phi_{laj}(\vec{k}) \Phi_{ok}(\vec{k}') + \\ P_{akl}(\vec{k}) \Phi_{akl}(\vec{k}') \Phi_{li}(\vec{k}'') + \\ P_{kac}(\vec{k}') \Phi_{aci}(\vec{k}'') \Phi_{aj}(\vec{k})$$

page 7  $\star$  This is a general property of turbulence we will revisit

where  $P_{\alpha\beta}(\vec{k}) = k_\alpha \delta_{\alpha\beta}(\vec{k}) + K_\alpha \delta_{\beta\alpha}(\vec{k})$  and

$$\Delta_{\alpha\beta}(\vec{k}) = \delta_{\alpha\beta} - k_\alpha k_\beta / k^2$$

To simplify things, we'll just write

$$[\partial_t + \nu(k^2 + k'^2 + k''^2)] \Phi_{ijk} = \sum_{QN} \Phi_{ij} \Phi_{ik} \quad (8)$$

When (8) was first derived, the community was excited, but it suffers the same problems as the previous QN closure we discussed. Importantly, it leads to significant negative values in the energy spectrum. That QN fails isn't very surprising since the joint PDFs are typically far from Gaussian. Part of the reason for the failure is that the QN theory builds in an arrow of time [Orszag (1970)]. Obviously, a viscous fluid is irreversible, but Orszag argued that even inviscid fluids should be statistically irreversible since on average they lead to greater mixing as time proceeds. So, he proposed adding an eddy viscosity to the 3rd order equation, creating the eddy damped QN (EDQN) closure,

$$[\partial_t + \nu(k^2 + k'^2 + k''^2) + \mu(\vec{k}) + \mu(\vec{k}') + \mu(\vec{k}'')] \Phi_{ijk} = \sum_{QN} \Phi_{ij} \Phi_{ik}$$

where  $\mu(\vec{k}) \sim [k^3 E(k)]^{1/2}$  (same as we derived for

turbulent diffusion in lecture III)

or sometimes  $\mu(\vec{k}) \sim \left[ \int_0^k k'^2 E(k') dk' \right]^{1/2}$ .

With this modification, the EDQN model is irreversible even when  $\nu = 0$ .

Another point EDQN addresses is the following:

In QN, for  $\nu$  small and  $k$  not too large ( $k < k_\nu$ )



$\Phi_{\vec{0};k} = \int_0^t \sum_{QN} \Phi_{\vec{0};j} \Phi_{\vec{0};j} d\tau$ , which implies that the instantaneous triple correlation depends on the entire history of the double correlation product. This is not very plausible. If we rewrite the EDQN closure as

$$\underbrace{[\partial_t + 1/\theta]}_{\text{all viscous terms}} \Phi_{\vec{0};k} = \sum_{QN} \Phi_{\vec{0};j} \Phi_{\vec{0};j}, \text{ then}$$

$\Phi_{\vec{0};k} = \int_0^t [\exp[(t-\tau)/\theta] \sum_{QN} \Phi_{\vec{0};j} \Phi_{\vec{0};j}] d\tau$ . This makes it clear that in the EDQN closure  $\Phi_{\vec{0};k}$  only depends on the immediate history of  $\Phi_{\vec{0};j}$ ,  $\Phi_{\vec{0};j}$  and that  $\theta$  is equivalent to the relaxation time. Note that  $\theta$  is always of order the eddy turnover time.

An alternate way to view the  $\mu$  terms are as a model for the 4th order cumulant terms discarded in QN theory, i.e., the joint PDFs are no longer purely Gaussian.

But the EDQN model still fails to guarantee that the energy spectrum remains positive! Orszag "fixed" this in the late seventies by Markovizing the EDQN model -- this just means to remove the memory of the system so that the conditional PDFs of future states depend only on the present state. So, the EDQNM drops the time derivative of  $\Phi_{\vec{0};k}$  leaving

$$[\nu(k^2 + k'^2 + k''^2) + \mu(k) + \mu(k') + \mu(k'')] \Phi_{\vec{0};k} = \sum_{QN} \Phi_{\vec{0};j} \Phi_{\vec{0};j}$$

This model finally gets the spectrum correct and is somewhat justifiable for small, fast eddies compared to larger, slower eddies.  $\therefore$  EDQNM

should not be applied to the energy containing range. EDQNM is still very popular and remains one of the best closure models. Two other popular, advanced models are the direct-interaction-approximation (DIA) [Kraichnan (1959)] (it doesn't even get the correct  $k^{-6/3}$ , though) and the test field model (TFM). TFM is very similar to EDQNM, but it uses an auxiliary (test) field to evaluate  $\Theta$ .

In summary, there are many ways to close the 1pt and 2pt equations, and they all work to varying degrees, but they all also suffer serious deficiencies.

### Further reading

- 1) P. A. Davidson "Turbulence" This book covers all of the closures discussed (and more) in more detail.
- 2) M. Lesieur "Turbulence in Fluids" covers the EDQNM closure in great detail. You can also get a free digital copy from the UMD library website

## VI Intermittency

Up to this point, we have adopted the clean picture of turbulence presented in K41. In reality self-similarity, homogeneity, and constant cascade rates do not hold. All of this is related to the concept of intermittency. Before we discuss intermittency, we need to establish some basic tools.

### A) Probability density functions

Since we are now going to be discussing turbulence in a more purely statistical sense, we will be using the probability density (or distribution) function,  $f$ , of a random variable, in our case the velocity,  $u$ . The probability  $u \in (a, b)$  is given by:

$$P(a < u < b) = \int_a^b f(u) du \quad \text{and} \quad \int_{-\infty}^{\infty} f du = 1$$

Effectively,  $f$  contains all of the information about the turbulence. Using  $f$ , we can construct some very important quantities:

$$\text{Mean } \mu = \int_{-\infty}^{\infty} u f du = \langle u \rangle$$

$$\text{Variance } \sigma^2 = \int_{-\infty}^{\infty} (u - \mu)^2 f du$$

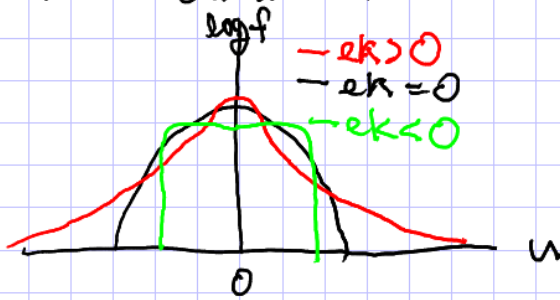
or if we consider only distributions with  $\mu = 0$ , which is a standard convention and what we use moving forward

$$\sigma^2 = \int_{-\infty}^{\infty} u^2 f du = \langle u^2 \rangle \quad \text{This measures the spread of the data}$$

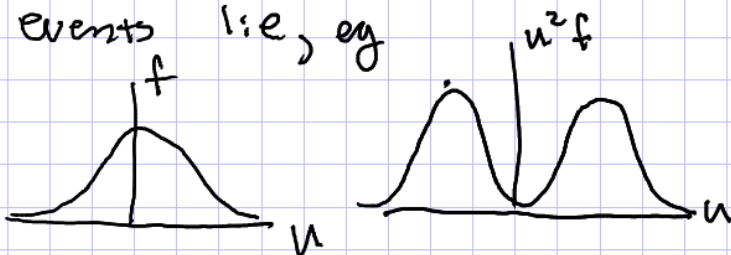
Skewness  $S = \frac{\int_{-\infty}^{\infty} u^3 f du}{\sigma^3} = \frac{\langle u^3 \rangle}{\langle u^2 \rangle^{3/2}}$  This measures the asymmetry of  $f$ . It is the first moment that actually tells us something about the shape of  $f$ . Note skew

page 2 a unimodal distribution can still be asymmetric but have  $S=0$  if for instance the left tail is long and thin and the right tail is short and fat such that they have the same area.

Flatness or kurtosis  $K = \frac{\int_{-\infty}^{\infty} u^4 f du}{\sigma^4} = \frac{\langle u^4 \rangle}{\langle u^2 \rangle^2}$  This measures the flatness or peakedness of  $f$  — this also effectively gives us information about the flatness of the tails. A normal distribution has  $K=3$ , so a quantity called excess kurtosis is often defined as  $e_k = K - 3$  for comparison with normal distributions.  $e_k < 0$  are called platykurtic and  $e_k > 0$  are leptokurtic (heavier tails than Gaussian).



Arbitrarily high order moments can be constructed but may not be finite (In fact, even those described above can diverge). The higher the moment of  $f$ , the more weight is given to the tails of  $f$ , where infrequent events lie, eg



Completely analogous quantities to those above can be defined for velocity increments,  $\delta u(r) = u(x+r) - u(x)$ .

page 2 Further, in the limit  $r \rightarrow 0$ , the same quantities

exist for derivatives, eg,

$$S(r \rightarrow 0) = S_0 = \frac{\langle \delta u^3 \rangle}{\langle \delta u^2 \rangle^{3/2}} = \frac{\langle (\partial u / \partial x)^3 \rangle}{\langle (\partial u / \partial x)^2 \rangle^{3/2}}$$

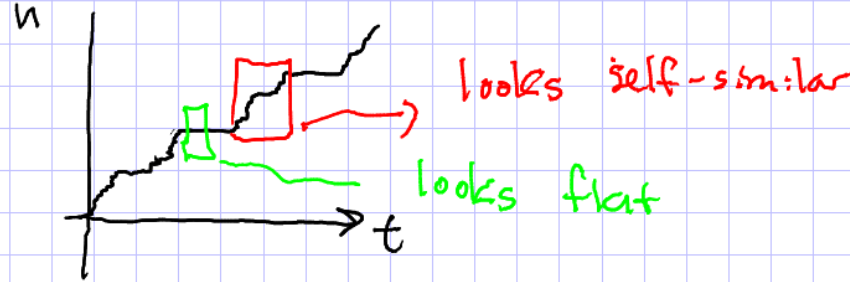
B Intermittency

Now that we have the tools, lets examine intermittency

We all know intuitively what intermittency means. If a process is self-similar, eg, Brownian motion, it is not intermittent

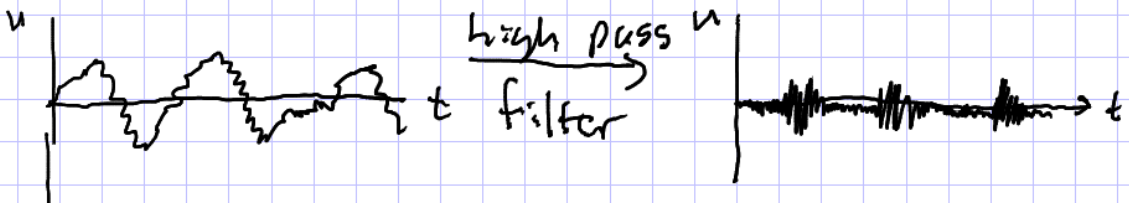


A classic intermittent example is the devil's staircase



The smaller the fragment we examine, the more likely it will be flat.

An intermittent signal could be "hiding" in data that looks self-similar



This is how intermittency in turbulence was identified, and related to one way to define intermittency

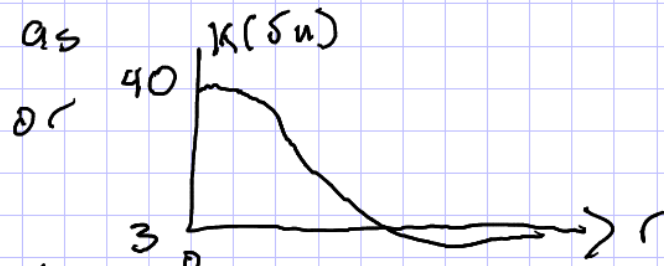
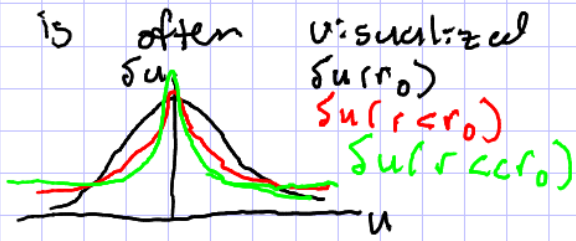
$$u(t) = \int_{\mathbb{R}} d\omega e^{i\omega t} u(\omega) \leftarrow \text{full FT}$$

$$u_{\Omega}^{\geq}(t) = \int_{\omega_{\Omega}} d\omega e^{i\omega t} u(\omega) \leftarrow \text{high pass FT}$$

then a signal is intermittent if

$$K(\Omega) = \frac{\langle u_{\Omega}^{\geq}(t)^4 \rangle}{\langle u_{\Omega}^{\geq}(t)^2 \rangle^2} \text{ grows without bound with } \Omega$$

page 4 In practice, it's more common to use structure functions since they already have a scale associated with them. Note that  $f(u)$  is actually very close to Gaussian because the value of  $u$  at any particular point is largely determined by chance. However, either filtered  $u$  or more commonly  $\delta u(r)$  is highly non-Gaussian for large  $R$  or small  $r$ . This

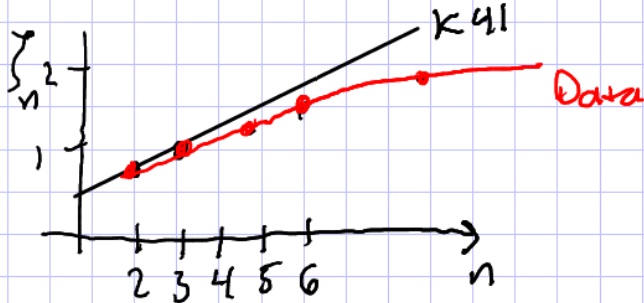


is often visualized as  $P(\delta u)$  or  $P(\delta u)$  the non-Gaussian nature of  $\delta u$  follows because it is related to the local dynamics

As noted above, the higher order the moment considered, the more focused is the quantity on the tails, which is where the extreme/intermittent events live. So, we can also look for intermittency by

looking at scaling exponents of the structure functions:

$$S_n(r) = \langle |\delta u - \bar{u}|^n \rangle \sim r^{\zeta_n} \quad \text{for } l_p \ll r \ll L$$



Note that:  $\zeta_n$  vs  $n$  must be both concave and non-decreasing (Frisch §9.4).

the  $4/5$  law tells us that  $\langle \delta u^3 \rangle = S_3(r) = -\frac{4}{5} \epsilon r$

$\Rightarrow \zeta_3 = 1$ . Note that the  $4/5$  law also

implies that the skewness of turbulence must be negative, which immediately  $\Rightarrow$  that  $f$  is not

Gaussian.

page 5 i) The K41 prediction

K41 assumes self-similarity  $\Rightarrow \delta u(\lambda r) = \lambda^h \delta u(r)$

$\Rightarrow S_n(\lambda r) = \lambda^{hn} S_n(r) \forall n$ . Well, we know

$$S_3 = -\frac{4}{5} \epsilon r \quad \therefore h = \frac{1}{3} \text{ and } S_n = n/3. \text{ Thus,}$$

we get the straight line in the  $S_n$  vs  $n$  figure

for K41. This is also referred to as being monofractal, eq.,

1 vertex always splits into two (self-similarity), which is equivalent

to  $\epsilon_r = \text{constant}$ .

ii) Refined Similarity [Kolmogorov 1962 (K62)]

We could consider a modification of K41 based on

intermittency, which is related to the volume or time

filling of the field. So, let's consider the possibility that

$S_n$  originates from just some fraction of the volume,

$$\chi_r^{(n)} \sim \left(\frac{r}{L}\right)^{M_n} \text{ then}$$

$$S_n(r) = \langle \delta u_r^n \rangle \sim \delta u_r^n \chi_r^{(n)} \sim (\epsilon r)^{n/3} \left(\frac{r}{L}\right)^{M_n} \sim \epsilon^{n/3} L^{-M_n} r^{\frac{n}{3} + M_n}$$

$$\Rightarrow S_n = \frac{n}{3} + \mu_n \quad (\mu_n \text{ must be a function of } n$$

since otherwise,  $S_3 = 1 \Rightarrow \mu = 0$ ).

Kolmogorov in 1962 explained the origin of the lack of

volume filling as follows

Consider an energy flux at a given scale

$$\epsilon_r(\vec{x}) = \frac{1}{3\pi r^3} \int_{|\vec{x}' - \vec{x}| < r} d\vec{x}' \nu |\nabla u(\vec{x}')|^2 \quad \text{By this definition,}$$

$\langle \epsilon_r \rangle = \epsilon = \text{traditional (K41) energy flux}$

Such local energy flux would be the case if dissipation

primarily occurs on filamentary structures.

If there is a local energy flux, then  
 $\delta u_r \sim (E_r r)^{1/3}$  rather than  $\delta u_r \sim (E r)^{1/3} \approx 1241$ ,  
 $\langle E_r^n \rangle = E^n \left(\frac{r}{L}\right)^{\mu_n}$ , where  $\mu_1 = 0$   
 $S_{u_r(r)} = \langle \delta u_r^n \rangle \sim \langle (E_r r)^{n/3} \rangle = \langle E_r^{n/3} \rangle r^{n/3} = E^{n/3} L^{-\mu_n/3} r^{\frac{n}{3} + \mu_n}$   
 $\therefore \zeta_n = \frac{n}{3} + \mu_n$ , where  $\mu_n$  is the scaling exponent for  
 $E_r$ . This is the refined similarity hypothesis.

Since  $E_r$  is no longer constant, we are now  
 considering multi-fractal<sup>\*</sup> turbulence and global scale  
 invariance has become local, i.e.,  $\delta u_{\lambda r} = \lambda^{h(r)} \delta u_r$   
 (loosely,  $h$  actually depends on the fractal dimension)

\* Turbulence can be seen to be multi-fractal from the  $\zeta_n$   
 vs  $n$  plot. Each time the fractal dimension changes, the slope of  
 the figure changes. Since it is a roughly smooth curve,  
 it is referred to as multi-fractal (continuous spectrum  
 of fractal dimensions).

### c) Modelling Intermittency

Now that we know turbulence is intermittent, let's  
 develop a way to model and describe the intermittency.  
 To do so, we'll use the simplest and first model  
 developed

#### The Random Cascade Model

Consider a system of size  $L$ , then  $\langle E_L \rangle = E$ . Now,  
 divide the box into smaller boxes of size  $\alpha L$ ,  $\alpha < 1$ .  
 Then, because of intermittency, we can say that  
 $E_{\alpha L} = E W_1$ , where  $W_1$  is a random variable,  $W_1 \geq 0$   
 and  $\langle W_1 \rangle = 1$  because  $\langle E_{\alpha L} \rangle = E$ . Now, divide the



boxes again  $E_{\alpha^2 L} = E_{\alpha L} W_2 = E W_1 W_2$ , where  $W_2$  is independent of  $W_1$ , but distributed the same  $\langle E_{\alpha^2 L} \rangle = E$ . Continuing to divide to a scale  $l = \alpha^k L$ ,  $E_e = E W_1 W_2 \dots W_k$ ,  $\langle E_e \rangle = E$ . Then  $\langle E_e^m \rangle = E^m \langle (W_1 \dots W_k)^m \rangle = E^m \langle W_1^m \rangle \dots \langle W_k^m \rangle$

but the  $W_i$ s are all distributed in the same way and  $l = \alpha^k L \Rightarrow k = \log_{\alpha}(\frac{l}{L})$ , so  $\langle E_e^m \rangle = E^m \langle W^m \rangle^k = E^m \alpha^{k \log_{\alpha} \langle W^m \rangle} = E^m \left(\frac{l}{L}\right)^{\mu_m \log_{\alpha} \langle W^m \rangle}$

$\therefore \langle E_e^m \rangle = E^m \left(\frac{l}{L}\right)^{\mu_m}$ , where  $\mu_m = \log_{\alpha} \langle W^m \rangle = \frac{\ln \langle W^m \rangle}{\ln \alpha}$

Applying this model to K41,  $W=1$  and  $\mu_m = 0$ .

To model intermittency on K62, we need to figure out how  $W$  is distributed.

First, our choice of  $\alpha$  must not influence the result, so replacing  $\alpha$  by  $\alpha^p$ ,  $p \in \mathbb{Z}^+$ , shouldn't change the result  $\Rightarrow W_1$  and  $W_1 \dots W_p$  must have the same distribution. If we define  $w_i = \ln W_i$ , then  $\sum_{i=1}^p w_i$  must have the same distribution as  $w_i$ , because  $W_1 \dots W_p = e^{\sum_{i=1}^p w_i}$  has the same distribution as  $W_i$ .

i) Lognormal Model

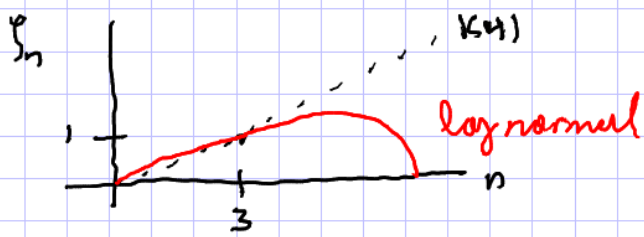
An obvious candidate distribution is the gaussian,  $f(w) = \frac{1}{\sqrt{2\pi}\sigma^2} e^{-\frac{(w - \langle w \rangle)^2}{2\sigma^2}}$ . Then,  $\sum_{i=1}^p w_i$  is also gaussian with mean  $p\langle w \rangle$  and variance  $p\sigma^2$ ,  $\therefore E_e$  is lognormal (Obukhov 1962)  $\langle W^m \rangle = \langle e^{mw} \rangle = \int dw e^{mw} f(w) = \frac{1}{\sqrt{2\pi}\sigma^2} \int dw e^{mw - \frac{(w - \langle w \rangle)^2}{2\sigma^2}} = e^{m\langle w \rangle + \frac{\sigma^2 m^2}{2}}$

We know that  $\langle W \rangle = 1$ , so  $\langle w \rangle + \frac{\sigma^2}{2} = 0$

$\Rightarrow \langle W^m \rangle = e^{\langle w \rangle m + \frac{\sigma^2 m^2}{2}} = e^{-\frac{\sigma^2 m^2}{2}}$

Recall that  $\mu_m = \frac{\ln \langle W^m \rangle}{\ln \alpha} = \frac{\langle w \rangle}{\ln \alpha} m(1-m)$   
 free parameter =  $\frac{\mu}{2}$

$$\therefore \zeta_n = \frac{n}{3} + \mu_{n/3} = \frac{n}{3} + \frac{\mu}{18} n(3-n)$$



This is not good, since we know  $\zeta_n$  is monotonic

### ii) Log Poisson (Sire - Lévêque 1994)

Another candidate distribution is the Poisson distribution:  $f(q) = \text{Probability}(X=q) = \frac{\lambda^q e^{-\lambda}}{q!}$ ,

where  $q=0,1,2,\dots$ ,  $\lambda \in \mathbb{R}$ ,  $\lambda > 0$ ,  $\lambda = \langle q \rangle = \langle q^2 \rangle^{1/2}$  and  $X$  is a discrete random variable.

This distribution  $\Rightarrow w = q \ln \beta + w_0$  ( $W = e^{w_0} \beta^q$ )

where  $\beta$  and  $w_0$  are parameters.

It is now log Poisson

$$\begin{aligned} \langle W^m \rangle &= \langle e^{mw} \rangle = \sum_{q=0}^{\infty} e^{mq \ln \beta + mw_0 - \lambda} \left( \frac{\lambda^q}{q!} \right) \\ &= e^{mw_0 - \lambda} \sum_{q=0}^{\infty} \underbrace{\frac{(\lambda \beta^m)^q}{q!}}_{e^{\lambda \beta^m}} = e^{mw_0 - \lambda(1-\beta^m)} \end{aligned}$$

$$\langle W \rangle = 1 \Rightarrow w_0 - \lambda(1-\beta) = 0 \text{ or } \lambda = \frac{w_0}{1-\beta}$$

$$\therefore \langle W^m \rangle = e^{w_0 \left( m - \frac{1-\beta^m}{1-\beta} \right)} \quad \text{and}$$

$$\mu_m = \frac{\ln \langle W^m \rangle}{\ln \alpha} = \frac{w_0}{\ln \alpha} \left( m - \frac{1-\beta^m}{1-\beta} \right) \Rightarrow$$

$$\zeta_n = \frac{n}{3} + \mu_{n/3} = \frac{n}{3}(1-x) + x \frac{1-\beta^{n/3}}{1-\beta}$$

$x$  and  $\beta$  are both parameters to determine

Note that  $\xi_n$  is monotonic for  $\beta < 1$

Let's now see if we can figure out values for  $\beta$  and  $x$ :

well,  $\langle \epsilon_e^m \rangle = \epsilon^m \left( \frac{\ell}{L} \right)^{-x(m - \frac{1-\beta^m}{1-\beta})}$

If we consider  $m \rightarrow \infty$ , then

$$\langle \epsilon_e^m \rangle \sim \epsilon^m \left( \frac{\ell}{L} \right)^{-xm + \frac{x}{1-\beta}} \quad (1)$$

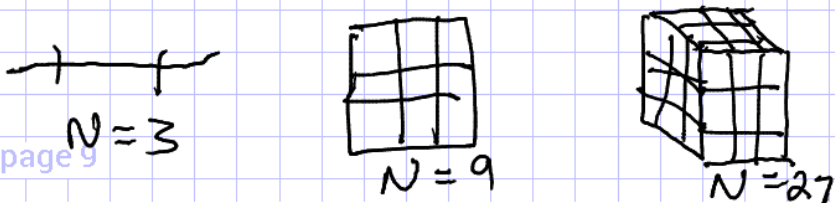
Remember that the higher the order of the moment considered, the more focused the quantity is on the extreme, i.e. singular, structures. So,

$$\langle \epsilon_e^m \rangle \underset{m \rightarrow \infty}{\sim} \left[ \epsilon_e^{(\infty)} \right] \chi_e$$

$\uparrow$  power dissipated in these structures       $\leftarrow$  volume filling fraction of the structures

$\chi_e$  must thus be of the form  $\chi_e \sim \left( \frac{\ell}{L} \right)^{d-D}$ , where  $d$  is the dimension of the embedding space considered ( $d=3$ ) and  $D$  is the dimension of the most singular structures.  $D$  is the fractal dimension and  $d-D$  is called the codimension,  $C$ .

Aside on fractal dimension: It is a ratio that provides a statistical index of complexity describing how detail changes with scale. The easiest intuitive picture is this:  $N \propto \epsilon^{-D}$ , where  $N$  is the # of new components,  $\epsilon$  is the scaling factor, and  $D$  is the fractal dimension. So, consider dividing a line, a rectangle and a box by thirds,  $\epsilon = 1/3$



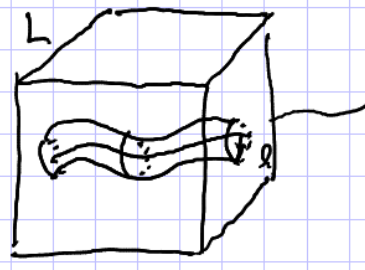
So,  $D=1$  for the line  
 $= 2$  for the rectangle  
 $= 3$  for the box

page 10 Note that  $D$  need not be an integer.

Back to original discussion

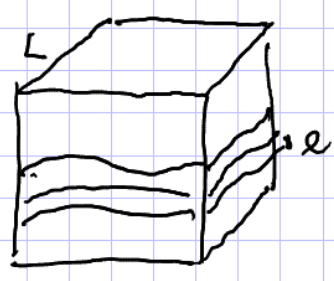
$\chi_e \sim \left(\frac{e}{L}\right)^{d-D}$  follows from it describing the probability for a ball of radius  $e$  to intersect with a dissipative structure for  $e \rightarrow 0$  (Also see alternate derivation). In  $d=3$ :

Filaments



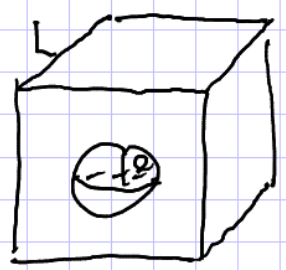
Volume  $\sim e^2 L \Rightarrow$   
 $\chi_e \sim \frac{e^2 L}{L^3} \sim \left(\frac{e}{L}\right)^{2=d-D} \Rightarrow D=1$   
 $C=2$

Sheets



Volume  $\sim e L^2 \Rightarrow$   
 $\chi_e \sim \frac{e L^2}{L^3} \sim \left(\frac{e}{L}\right)^1 \Rightarrow D=2$   
 $C=1$

Spheres



Volume  $\sim e^3 \Rightarrow$   
 $\chi_e \sim \left(\frac{e}{L}\right)^3 \Rightarrow D=0$   
 $C=3$

Note that  $D$  need not be an integer

$\therefore \langle E_e^{(m)} \rangle \sim [E_e^{(\infty)}]^{(m)} \left(\frac{e}{L}\right)^C$  and  $(1) \Rightarrow$

$\langle E_e^{(m)} \rangle \sim \left[e \left(\frac{e}{L}\right)^{-x}\right]^m \left(\frac{e}{L}\right)^{\frac{x}{1-\beta}}$

$\therefore E_e^{(\infty)} \sim e \left(\frac{e}{L}\right)^{-x}$  and  $\frac{x}{1-\beta} = C$  and

$\zeta_m = (1-x)\frac{m}{3} + C \left[1 - \left(1 - \frac{x}{C}\right)^{m/3}\right]$

The Lévésgre assumed that most of the energy on the cascade is dissipated in these singular structures and that the cascade time obeys the K41 scaling

$E_e^{(\infty)} \sim \frac{U_0^2}{\tau_e} \sim U_0^2 e^{1/3} L^{-2/3} \Rightarrow x = 2/3$

We know empirically that the primary dissipative structures are filaments, so  $C=2$

$$\therefore \zeta_n = \frac{n}{9} + 2 \left[ 1 - \left( \frac{2}{3} \right)^{n/3} \right] \quad \text{Log-Poisson model}$$

This fits the experimental data well

### D Extended Self-Similarity (Benzi et al 1993)

measuring high order  $S_n$  can be difficult for only moderate  $Re$ . So, Benzi et al 1993 created a trick: since  $S_3(r) \sim r$ , why not measure

$S_n(r)$  vs  $S_3(r)$  rather than  $S_n(r)$  vs  $r$ ?

this approach  $\Rightarrow S_n(r) \sim r^{\zeta_n} \sim S_3(r)^{\zeta_n}$ .

$$\therefore \zeta_n = \frac{\partial \ln S_n(r)}{\partial \ln S_3(r)}$$

This works because the "noise" in the structure functions is correlated across all orders. So, it effectively cancels using this method. The method is called extended self-similarity because it cures the lack of asymptotic present due to the low Reynolds number by observing that the functional form of the structure functions is the same at the beginning of the dissipation range.

### Alternate derivation of $\chi_{\ell}$

$$\chi_{\ell} = N \frac{\ell^d}{L^d} \sim \left( \frac{\ell}{L} \right)^D \left( \frac{\ell}{L} \right)^d = \left( \frac{\ell}{L} \right)^{d-D}$$

, where  $N$  is the # of eddies of size  $\ell$  and I used  $N \sim \epsilon^{-D}$  with  $\epsilon =$  the scaling factor  $= \frac{\ell}{L}$